

Curvature of attached shock waves in steady axially symmetric flow

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An electronic computer has been employed to calculate the ratio between the initial radii of curvature of the attached shock wave and the body for an axially symmetrical body in a uniform supersonic stream. The results are obtained with 4 exact digits for more than 200 cases. They extend results obtained previously (Cabannes 1951) by means of numerical integration.

1. Introduction

We consider a body of revolution placed in a compressible fluid. The fluid possesses at infinity a uniform supersonic velocity \bar{q} parallel to the axis of revolution Ox . A shock wave is formed in front of the body, and limits the region in

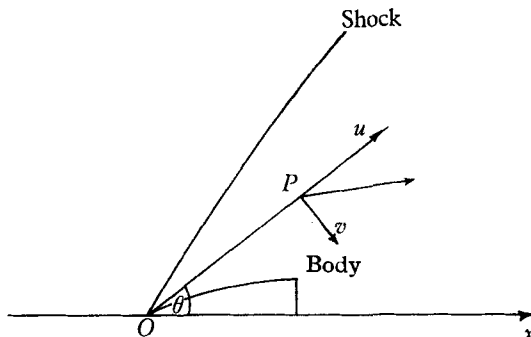


FIGURE 1. Diagram of the flow field.

which the flow is uniform. Viscosity and thermal conductivity are neglected outside the shock. We suppose that the surface of the body is tangential at the axis of revolution to a cone with semi-angle θ_s , and that the angle θ_s and the Mach number M of the upstream flow have been chosen in such a way that the shock wave is attached at the vertex O of the obstacle. We locate the position of a point P in a meridional plane by the polar co-ordinates $OP = r$ and $\angle POx = \theta$ (see figure 1). By means of these co-ordinates, the equation of the obstacle in the neighbourhood of the point O can be written in the form (1) and the equation of the shock wave, in the neighbourhood of the same point, in the form (2), namely,

$$\text{body: } \theta = \theta_s + \frac{r}{2R} + \dots, \quad (1)$$

$$\text{shock: } \theta = \theta_w + \frac{r}{2R} + \dots \quad (2)$$

The angle θ_w is determined by the theory of axially symmetric flow (Kopal 1947); it depends on the Mach number M and the angle θ_s . The object of the present paper is to give tables for the determination of the value of the ratio (R/\mathcal{R}) of the radii of curvature, at the axis of revolution, of the shock wave and the body; this ratio likewise depends on the Mach number M and the angle θ_s .

2. Equations of motion

We designate by u and v the components of the fluid velocity at a point P in the directions θ and $(\theta + \frac{1}{2}\pi)$, by p and ρ the pressure and density at this point, and by γ the ratio of the specific heats of the fluid. The four functions u , v , p and ρ of the variables r and θ satisfy the following partial differential equations which express the fundamental law of dynamics, the conservation of mass and the conservation of energy :

$$\left. \begin{aligned} u \frac{\partial u}{\partial r} + \frac{v}{r} \frac{\partial u}{\partial \theta} - \frac{v^2}{r} + \frac{1}{\rho} \frac{\partial p}{\partial r} &= 0, \\ u \frac{\partial v}{\partial r} + \frac{v}{r} \frac{\partial v}{\partial \theta} + \frac{uv}{r} + \frac{1}{\rho r} \frac{\partial p}{\partial \theta} &= 0, \\ \frac{\partial}{\partial r} (r^2 \rho u \sin \theta) + \frac{\partial}{\partial \theta} (r \rho v \sin \theta) &= 0, \\ u \frac{\partial}{\partial r} (p \rho^{-\gamma}) + \frac{v}{r} \frac{\partial}{\partial \theta} (p \rho^{-\gamma}) &= 0. \end{aligned} \right\} \quad (3)$$

We attempt to satisfy the preceding equations by means of functions expanded in series of whole and increasing powers of r , the coefficients depending only on the variable θ :

$$\left. \begin{aligned} u(r, \theta) &= u_0(\theta) + \frac{r}{R} u_1(\theta) + \dots, \\ v(r, \theta) &= v_0(\theta) + \frac{r}{R} v_1(\theta) + \dots, \\ p(r, \theta) &= p_0(\theta) + \frac{r}{R} p_1(\theta) + \dots, \\ \rho(r, \theta) &= \rho_0(\theta) + \frac{r}{R} \rho_1(\theta) + \dots \end{aligned} \right\} \quad (4)$$

By substitution of these expansions into equations (3) and by identification according to successive powers of r , one obtains an infinite set of differential equations. Equations (3) have a first integral, Bernoulli's equation. As the limiting speed q_m is constant in front of the shock and continuous across the shock wave, we have, valid in all the fluid,

$$\frac{2\gamma}{\gamma-1} \frac{p}{\rho} + u^2 + v^2 = q_m^2. \quad (5)$$

We also introduce the function $a_0(\theta)$ defined by:

$$a_0^2 = \gamma \frac{p_0}{\rho_0} = \frac{\gamma-1}{2} (q_m^2 - u_0^2 - v_0^2). \quad (6)$$

The differential equations deduced from equations (3) can be written in the following form. Using given initial conditions, the functions with suffix 0 can be calculated from equations (7), while the functions with suffix 1 can be calculated from equations (8):

$$\left. \begin{aligned} u'_0 - v_0 &= 0, \\ v'_0 \left(1 - \frac{a_0^2}{v_0^2} \right) + u_0 \left(1 - 2 \frac{a_0^2}{v_0^2} \right) - \frac{a_0^2}{v_0} \cot \theta &= 0, \\ \frac{\rho'_0}{\rho_0} \left(1 - \frac{a_0^2}{v_0^2} \right) + \frac{u_0}{v_0} + \cot \theta &= 0, \\ \frac{p'_0}{p_0} - \gamma \frac{\rho'_0}{\rho_0} &= 0. \end{aligned} \right\} \quad (7)$$

$$\left. \begin{aligned} u'_1 v_0 + u_0 u_1 - v_0 v_1 + \frac{a_0^2 p_1}{\gamma p_0} &= 0, \\ \left(\frac{\rho_1}{\rho_0} \right)' + \frac{v_0 v'_0}{a_0^2} + \frac{u_1 v_0 + v_1 (2u_0 + v'_0)}{a_0^2} \\ - \frac{\rho_1}{\rho_0} \left(\frac{\rho'_1}{\rho_0} - \frac{u_0}{v_0} \right) + \frac{p_1}{p_0} \left(\frac{\rho'_0}{\rho_0} - \frac{1}{\gamma} \frac{u_0}{v_0} \right) &= 0, \\ \left(\frac{\rho_1}{\rho_0} \right)' + \frac{v'_1}{v_0} + 3 \frac{u_1}{v_0} + \frac{v_1}{v_0} \left(\frac{\rho'_0}{\rho_0} + \cot \theta \right) + \frac{\rho_1 u_0}{\rho_0 v_0} &= 0, \\ \frac{p_1}{p_0} - \frac{\rho_1}{\rho_0} + (\gamma - 1) \frac{u_0 u_1 + v_0 v_1}{a_0^2} &= 0. \end{aligned} \right\} \quad (8)$$

3. Boundary conditions on the body

The body is formed by the stream surface extended from the point 0. By expressing the condition that the differential equation of the stream function,

$$\frac{dr}{u} = \frac{r d\theta}{v}, \quad (9)$$

is satisfied by the function (1), one obtains the conditions

$$v_0(\theta_s) = 0, \quad (10a)$$

$$\frac{v'_0(\theta_s)}{2\mathcal{R}} + \frac{v_1(\theta_s)}{R} = \frac{u_0(\theta_s)}{2\mathcal{R}}. \quad (10b)$$

According to the second of equations (7), one has that $v'_0(\theta_s) = -2u_0(\theta_s)$; therefore the condition (10b) can be written in the form

$$\frac{R}{\mathcal{R}} = \frac{2v_1(\theta_s)}{3u_0(\theta_s)}. \quad (11)$$

4. Conditions on the shock wave

At the shock wave, a certain number of conditions must be satisfied. These conditions, which express the fundamental law of dynamics, the conservation of mass and the conservation of energy, are expressed by equations (12), in which \bar{c} , \bar{p} and $\bar{\rho}$ designate the speed of sound, pressure and density in front of the shock

while β is the angle which the tangent to the shock wave makes with the axis of revolution. \mathcal{M} designates the Mach number along the normal ($\mathcal{M} = M \sin \beta$).

$$\left. \begin{aligned} u &= \bar{q} \cos \theta + \frac{2\bar{c}}{\gamma+1} \left(\mathcal{M} - \frac{1}{\mathcal{M}} \right) \sin(\beta - \theta), \\ v &= -\bar{q} \sin \theta - \frac{2\bar{c}}{\gamma+1} \left(\mathcal{M} - \frac{1}{\mathcal{M}} \right) \cos(\beta - \theta), \\ \frac{p}{\bar{p}} &= \frac{2\gamma}{\gamma+1} \mathcal{M}^2 - \frac{\gamma-1}{\gamma+1}, \\ \frac{\bar{\rho}}{\rho} &= \frac{2}{\gamma+1} \frac{1}{\mathcal{M}^2} + \frac{\gamma-1}{\gamma+1}. \end{aligned} \right\} \quad (12)$$

The Mach number M is expressed as a function of the speed \bar{q} by

$$M^2 = \frac{2}{\gamma-1} \frac{\bar{q}^2}{q_m^2 - \bar{q}^2}. \quad (13)$$

By expressing the fact that the equations (12) are satisfied identically on the shock wave, one obtains the following values for the functions with suffix 0 and 1 for $\theta = \theta_w$:

$$\left. \begin{aligned} u_0(\theta_w) &= \bar{q} \cos \theta_w, \\ v_0(\theta_w) &= \frac{\gamma-1}{\gamma+1} \frac{\bar{q}^2 \cos^2 \theta_w - q_m^2}{\bar{q} \sin \theta_w}, \\ \frac{p_0(\theta_w)}{\bar{p}} &= \frac{2\gamma}{\gamma+1} M^2 \sin^2 \theta_w - \frac{\gamma-1}{\gamma+1}, \\ \frac{\bar{\rho}}{\rho_0(\theta_w)} &= \frac{2}{\gamma+1} \frac{1}{M^2 \sin^2 \theta_w} + \frac{\gamma-1}{\gamma+1}; \end{aligned} \right\} \quad (14)$$

$$\left. \begin{aligned} u_1 + u_0 \tan \theta_w + v_0 &= 0, \\ 2v_1 + \frac{\gamma-7}{\gamma+1} u_0 + \frac{\gamma+3}{\gamma+1} v_0 \cot \theta_w &= 0, \\ \frac{p_1}{p_0} &= \frac{\gamma}{\gamma+1} \cot \theta_w - \frac{4\gamma}{\gamma+1} \frac{u_0 v_0}{a_0^2}, \\ \frac{\rho_1}{\rho_0} &= \frac{2\gamma+3}{\gamma+1} \cot \theta_w + 2 \frac{\gamma-1}{\gamma+1} \frac{u_0}{v_0}. \end{aligned} \right\} \quad (15)$$

5. Numerical integration

The numerical integration of equations (7) and (8) has been performed with the help of electronic computer gamma of the Faculty of Sciences of Grenoble. The great capacity of the machine and its high velocity of execution have allowed the computation of 209 cases to be performed, corresponding to 15 different bodies. The method of integration adopted is the Runge-Kutta method of fourth order, with intervals equal to one-twentieth of a degree; it seems that the value of the ratio of the curvatures can then be predicted with 4 exact digits. The results, which are given in the following tables,* have been computed with the adiabatic

* For $u_0(\theta_s)/q_m = (1/6)^{1/2} = 0.4082$, the speed on the body, at the vertex, is sonic.

index having the value $\gamma = 1.4$. The ratio of the curvatures is negative for the limiting velocity for which the shock wave is detached from the body; it is zero for a given value of the Mach number, which has been computed.

In the case where the angle θ_s is small, it can be verified that the asymptotic formula, given by Rao (1956),

$$\frac{R}{\mathcal{R}} \sim \frac{40}{81} \frac{1}{(\gamma + 1)^4} \frac{(M^2 - 1)^3}{M^{13}} \theta_s^{-7}, \quad (16)$$

is satisfactory for finite values of the Mach number. For higher values of θ_s , the results are exhibited graphically in figure 2.

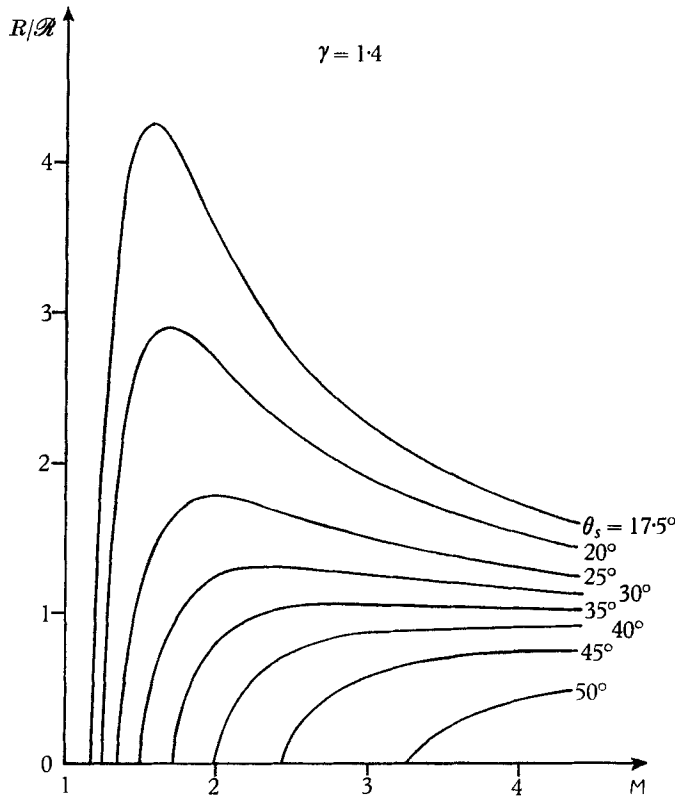


FIGURE 2. Values of R/\mathcal{R} vs M for various θ_s .

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$\frac{u_0(\theta_s)}{q_m}$	M	θ_w^*	R/\mathcal{R}	$\frac{u_0(\theta_s)}{q_m}$	M	θ_w	R/\mathcal{R}
$\theta_s = 5^\circ$				$\theta_s = 12.5^\circ$ (cont.)			
0.35	1.1732	89.224	-0.3234	0.4082	1.1674	61.593	7.3049
0.39	1.0215	86.921	-1.4832	0.45	1.2892	52.804	14.2637
0.3913	1.0180	86.441	-1.7700	0.5	1.4633	44.923	15.6587
0.395	1.0128	84.104	-2.2779	0.55	1.6623	38.934	13.1465
0.399	1.0168	80.841	6.0933	0.6	1.8916	34.144	10.0314
0.4	1.0187	80.072	10.4070	0.65	2.1618	30.176	7.4305
0.4082	1.0414	74.131	167.7417	0.7	2.4900	26.802	5.4927
0.55	1.5151	41.363	4759.00	0.75	2.9070	23.869	4.0938
0.6	1.7258	35.482	2196.71	0.8	3.4725	21.265	3.0785
0.65	1.9699	30.597	1172.21	0.85	4.3239	18.903	2.3215
0.7	2.2611	26.372	576.76	0.9	5.8910	16.709	1.7300
0.75	2.6224	22.592	255.98	0.95	11.1397	14.606	1.2335
0.8	3.0961	19.107	103.76	$\theta_s = 15^\circ$			
0.85	3.7723	15.792	29.586	0.3	1.2830	84.715	-1.0269
0.9	4.8895	12.527	12.9795	0.35	1.1196	75.231	-0.8898
0.95	7.4586	9.136	4.3398	0.3670	1.1289	70.070	0.0000
0.99	22.6254	5.992	1.3343	0.385	1.1608	64.965	1.6265
$\theta_s = 7.5^\circ$				0.4	1.1964	61.214	3.1447
0.36	1.0980	87.324	-0.6790	0.45	1.3448	51.391	6.6419
0.39	1.0334	78.125	0.6794	0.5	1.5224	44.289	7.2050
0.395	1.0420	75.455	6.1709	0.55	1.7271	38.827	6.3878
0.4	1.0529	73.030	15.591	0.6	1.9648	34.444	5.2728
0.4082	1.0766	69.063	43.683	0.65	2.2468	30.816	4.2547
0.45	1.1971	57.012	212.00	0.7	2.5928	27.738	3.4213
0.5	1.3657	47.360	281.44	0.75	3.0381	25.071	2.7579
0.55	1.5555	40.313	223.08	0.8	3.6541	22.712	2.2271
0.6	1.7715	34.729	145.74	0.85	4.6151	20.587	1.7922
0.65	2.0229	30.082	84.598	0.9	6.5337	18.630	1.4227
0.7	2.3244	26.080	46.690	0.95	16.8844	16.787	1.0793
0.75	2.7007	22.537	25.197	$\theta_s = 17.5^\circ$			
0.8	3.1985	19.326	13.516	0.3	1.2665	82.113	-1.1618
0.85	3.9177	16.348	7.3241	0.3582	1.1707	68.912	-0.1426
0.9	5.1329	13.505	3.9809	0.3611	1.1743	68.153	0.0000
0.95	8.1036	10.665	2.1041	0.4	1.2551	59.124	2.1327
0.98	16.8180	8.850	1.2883	0.45	1.4062	50.476	3.8682
$\theta_s = 10^\circ$				0.5	1.5881	44.067	4.2223
0.3765	1.0535	77.311	-0.8455	0.55	1.7996	39.089	3.9217
0.3810	1.0576	75.347	0.0000	0.6	2.0472	35.079	3.4297
0.4	1.0948	67.957	9.0936	0.65	2.3438	31.756	2.9338
0.4082	1.1190	64.899	15.9125	0.7	2.7122	28.939	2.4909
0.45	1.2398	54.713	42.7685	0.75	3.1947	26.502	2.1100
0.5	1.4109	45.976	49.7619	0.8	3.8809	24.355	1.7717
0.55	1.6049	39.445	39.7939	0.85	5.0080	22.430	1.4945
0.6	1.8271	34.238	27.6345	0.9	7.5793	20.699	1.2427
0.65	2.0872	29.915	18.1499	$\theta_s = 20^\circ$			
0.7	2.4009	26.220	11.8199	0.3	1.2728	79.220	-1.1975
0.75	2.7956	22.985	7.7432	0.356	1.2271	66.747	-0.0045
0.8	3.3231	20.093	5.1675	0.3561	1.2259	66.670	0.0000
0.85	4.0951	17.499	3.4898	0.4	1.3191	57.697	1.5749
0.9	5.4526	14.966	2.3434	0.4082	1.3452	56.068	1.8450
0.95	9.1471	12.541	1.5017	0.45	1.4737	50.008	2.6155
0.98	19.2181	11.048	1.0663	0.5	1.6609	44.205	2.8858
$\theta_s = 12.5^\circ$				0.55	1.8806	39.658	2.7762
0.3	1.3168	86.723	-0.8426	0.6	2.1404	35.980	2.5168
0.3738	1.0902	72.409	0.0249	0.65	2.4555	32.928	2.2497
0.4	1.1429	64.103	5.1224				

TABLE I

* The angles θ_w are given in degrees.

$\frac{u_0(\theta_s)}{q_m}$	M	θ_w	R/\mathcal{R}	$\frac{u_0(\theta_s)}{q_m}$	M	θ_w	R/\mathcal{R}
$\theta_s = 20^\circ$ (cont.)				$\theta_s = 35^\circ$ (cont.)			
0.7	2.8531	30.339	1.9759	0.3395	1.7105	64.316	0.0000
0.75	3.3862	28.105	1.7346	0.35	1.7309	63.009	0.1325
0.8	4.1742	26.141	1.5129	0.4	1.8766	57.548	0.6104
0.85	5.5710	24.391	1.3591	0.4082	1.9115	56.656	0.6745
0.9	9.6230	22.807	1.1805	0.45	2.0875	53.216	0.8793
$\theta_s = 22.5^\circ$				0.5	2.3633	49.758	1.0112
0.3	1.3014	76.482	-1.1329	0.55	2.7228	46.957	1.0635
0.3518	1.2840	65.538	0.0000	0.6	3.2112	44.653	1.0673
0.3520	1.2856	65.596	0.0057	0.65	3.9340	42.729	1.0473
0.4	1.3888	56.913	1.2413	0.7	5.2059	41.122	1.0160
0.4082	1.4157	55.363	1.4234	0.75	8.6893	39.706	0.9780
0.45	1.5479	49.920	1.9532	0.78	24.7546	38.964	0.8756
0.5	1.7418	44.643	2.1769	$\theta_s = 40^\circ$			
0.55	1.9718	40.476	2.1487	0.3	1.9533	69.453	-0.4848
0.6	2.2471	37.092	2.0138	0.3374	1.9938	65.177	-0.0107
0.65	2.5860	34.279	1.8415	0.3381	1.9982	65.147	0.0000
0.7	3.0229	31.894	1.6881	0.34	1.9993	64.902	0.0133
0.75	3.6274	29.837	1.4817	0.35	2.0235	63.863	0.1217
0.8	4.5707	28.036	1.3309	0.4	2.2027	59.282	0.5052
0.85	16.7401	25.002	1.0461	0.4082	2.2463	58.527	0.5565
$\theta_s = 25^\circ$				0.45	2.4712	55.606	0.7275
0.3	1.3484	74.181	-1.0138	0.5	2.8441	52.647	0.8455
0.3478	1.3487	64.913	-0.0089	0.55	3.3752	50.238	0.9019
0.3481	1.3493	64.841	0.0000	0.6	4.2147	48.299	0.9217
0.3489	1.3504	64.704	0.0174	0.65	5.8293	46.589	0.9201
0.35	1.3534	64.550	0.0427	0.7	12.8630	45.186	0.9114
0.4	1.4653	56.367	1.0250	0.711	27.3166	44.907	0.8763
0.4082	1.4931	55.066	1.1591	$\theta_s = 45^\circ$			
0.45	1.6299	50.146	1.5576	0.3	2.3720	70.058	-0.4205
0.5	1.8325	45.328	1.7465	0.32	2.3910	68.077	-0.1833
0.55	2.0757	41.497	1.7606	0.3383	2.4336	66.381	0.0000
0.6	2.3712	38.374	1.6849	0.34	2.4387	66.228	0.0154
0.65	2.7422	35.775	1.5724	0.35	2.4718	65.354	0.1017
0.7	3.2335	33.571	1.4482	0.4	2.7233	61.487	0.4271
0.75	3.9442	31.698	1.3211	0.4082	2.7866	60.847	0.4709
0.8	5.1439	30.018	1.2101	0.45	3.1279	58.360	0.6220
0.85	8.1165	28.5546	1.0877	0.5	3.7626	55.827	0.7311
0.9	27.9654	27.626	0.8890	0.55	4.8844	53.757	0.7937
$\theta_s = 30^\circ$				0.6	7.7892	52.046	0.8261
0.3	1.4857	71.094	-0.7675	0.633	26.2600	51.075	0.8640
0.3427	1.5058	64.163	0.0000	$\theta_s = 50^\circ$			
0.35	1.5180	63.068	0.1194	0.3	3.1392	71.261	-0.3833
0.4	1.6446	56.477	0.7645	0.32	3.1735	69.593	-0.1723
0.4082	1.6750	55.409	0.8509	0.3395	3.2539	68.078	-0.0012
0.45	1.8259	51.326	1.1179	0.3396	3.2546	68.067	0.0000
0.5	2.0546	47.265	1.2721	0.35	3.3154	67.302	0.0780
0.55	2.3390	44.050	1.3128	0.4	3.7916	64.038	0.3675
0.6	2.6971	41.325	1.2929	0.4082	3.9220	63.497	0.4078
0.65	3.1745	39.093	1.2410	0.45	4.7239	61.385	0.5445
0.7	3.8645	37.202	1.1786	0.5	7.0019	59.225	0.6520
0.75	5.0277	35.579	1.1085	0.54	21.4992	57.782	0.8512
0.8	7.8707	34.171	1.0384	$\theta_s = 55^\circ$			
0.835	24.0388	32.291	0.8803	0.3	5.4816	72.901	-0.3628
$\theta_s = 35^\circ$				0.35	6.2273	69.588	0.0576
0.3	1.6797	69.681	-0.5928	0.4	9.8838	66.850	0.3202
0.3391	1.7099	64.361	-0.0047	0.4082	12.0445	66.394	0.3573

TABLE I (cont.)